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(54) **A POLYOLEFIN ALLOY WITH IMPROVED SURFACE HARDNESS AND SCRATCH RESISTANCE,  
AND PROCESSES FOR PRODUCING SAME**

EINE POLYOLEFINLEGIERUNG MIT VERBESSERTER OBERFLÄCHENHÄRTE UND  
KRATZFESTIGKEIT, UND VERFAHREN ZU IHRER HERSTELLUNG

ALLIAGE POLYOLEFINIQUE AVEC UNE DURETE SUPERFICIELLE ET UNE RESISTANCE A LA  
RAYURE AMELIOREES, ET SES PROCEDES DE FABRICATION

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(Basic).**

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**EP 0 804 503 B1**

## Description

[0001] The present invention relates to a polyolefin alloy with improved surface hardness and scratch resistance, and processes for producing same. More specifically, the invention relates to a polyolefin alloy on the basis of a polypropylene material, a functionalized polypropylene material, a mineral, an amorphous silica gel and optionally an ethylene/propylene/polyene terpolymer (EPDM), as well as processes for producing said polyolefin alloy.

[0002] Various techniques for increasing the scratch resistance of polyolefin materials are previously known, i.e. addition of silica materials. Thus, JP 1318051 (Toray Silicone KK) discloses polyolefins which for this purpose have been modified with a filler on silica basis. Said filler may have been surface treated with silane type compounds. However, the disclosed polyolefins are not alloys and no fatty acid amide-treated silica gel is used in the material. JP 1104637 (Showa Denko KK) discloses materials on a polypropylene basis to which silica/alumina spheroids and a polypropylene material functionalized with carboxylic acid or carboxylic anhydride have been added. These materials also contains no fatty acid amide-treated silica gel.

[0003] It has now been found that when a functionalized polypropylene material and an amorphous, fatty acid amide-modified silica gel are incorporated into certain polyolefin materials having a mineral content, the scratch resistance of the material is substantially improved, with retention of the impact strength and the thermal shape stability (HDTA) of the material.

[0004] Thus, the invention provides a new polyolefin alloy having improved surface hardness and scratch resistance, and having a melt index MI in the range of 0.1 - 50 g/10 min at 230°C/2.16 kg, particularly in the range of 3 to 40 g/10 min at 230°C/2.16 kg. The polyolefin alloy is characterized in that it is constituted by a blend of:

(A) 40 to 80% by weight of a polypropylene material consisting of a polypropylene homopolymer or a copolymer of propylene with ethylene and/or butadiene, which polypropylene material may have a content of polymerized ethylene and/or butadiene units of 5 to 35 mole% and has a molecular weight Mw of 100,000 to 300,000 and a melt index MI of 0.1 to 20 g/10 min at 230°C/2.16 kg,

(B) 1 to 10% by weight of a functionalized polypropylene material consisting of a grafted polypropylene homopolymer or copolymer of propylene with ethylene and/or butadiene, having a degree of grafting of 0.2 to 10% by weight,

(C) 1 to 50% by weight of a mineral, having a mean particle size of about 2.5 µm and a maximum particle size of 20 µm, and being surface-treated with 0.2 to 5% by weight of aminosilane,

(D) 1 to 15% by weight of amorphous fatty acid-treated silica gel, comprising 25 to 75% by weight of silica and 75 to 25% by weight of fatty acid amide,

(E) 0 to 40% by weight of an ethylene/propylene/polyene terpolymer (EPDM) having a melt index MI in the range of 1 to 10 g/10 min at 230°C/2.16 kg and a Shore D hardness of 30 to 70.

[0005] EP-A-O 567 058 (Hirano et al.) discloses compositions having improved elasticity, peeling strength and re-coating properties, comprising a polypropylene, an ethylene/a-olefin copolymer elastomer, and a modified polyolefin having a functional group in either or both ends thereof, as well as certain substituted amines/amides. In addition thereto, the compositions can also contain various additives, among which talc is mentioned. Said compositions of EP-A-O 567 058 do not, however, contain the combination of a functionalized polypropylene material of the same kind as component (B) of the polyolefin alloy of the present invention, with a mineral having been surface-treated with an aminosilane, and a fatty acid-treated silica gel, and they do not suggest any improvement of the scratch resistance.

[0006] US 4 675 122 (Lüers et al.) teaches a combined antiblocking agent and lubricant concentrate based on polyolefin, which contains diatomaceous earth, precipitated silica and/or silica gel as the antiblocking agent, and one more more amides of unsaturated C<sub>18</sub>-C<sub>22</sub> fatty acids. No mention is made of any improvement of the scratch-resistance. Also, it could not be considered to be near at hand to combine the teaching of US 4 675 122 with the teaching of the above-discussed EP-A-O 567 058, which also does not mention scratch-resistance.

[0007] EP-A-O 297 693 (McKinney et al.) teaches a composition comprising an intimate mixture of at least one ethylene interpolymer with acrylic acid, methacrylic acid or an ionomer of either of said acids and a slip-enhancing amount of a secondary fatty acid amide. The composition may also contain small amounts of finely divided inorganic materials such as silica and talc. The aim of the invention of EP-A-O 297 693 is to improve the slip and/or block characteristics of the ethylene interpolymers. No mention is made of any improvement of the scratch-resistance. Even though said EP-A-O 297 693 is disclosing compositions in which silica may be used, and will come into contact with fatty acid amide, it is not question there of any fatty acid-treated silica gel comprising 25-75% by weight of silica and 75-25% by weight of fatty acid amide as in the polyolefin alloy of the present invention. To the extent a finely inorganic material is used in the composition of EP-A-O 297 693, no surface treatment thereof with aminosilane is mentioned, neither is there any mention of any functionalized polypropylene material. A similar composition is disclosed in EP-A-O 257 803 (Yamada et al.), comprising an ethylene/methyl methacrylate copolymer, a slip agent which may be a fatty acid amide, and a small amount (0.01-0.1 %wt) of an inorganic filler, which may be a silica or a talc. The composition is used to

produce peelable protective films with low peeling strength for wrapping around e.g. rubbery articles having a tacky surface. Neither EP-A-O 257 803 nor EP-A-O 297 693 suggests the polyolefin alloy of the present invention having improved surface hardness and scratch-resistance.

**[0008]** US 5 286 791 (De Nicola et al.) discloses a filled composition having improved flexural modulus and impact strength, comprising a propylene polymer material, a propylene polymer material grafted with one or more vinyl monomers, and a rubber component. As filler, the composition may contain i.a. talc and silica, and column 3, lines 25-37, of the patent indicates that the filler may be coated with an organic compound. However, the patent does not suggest any fatty acid amide-treated silica gel in combination with an aminosilane-treated mineral and there is no suggestion in said patent that any such combination would improve the surface hardness and scratch-resistance of a polyolefin alloy as defined according to the present invention.

**[0009]** The new polyolefin alloy of the present invention can be produced by blending the components (A), (B), (C) and (D), and optionally utilized component (E); melting and preferably kneading the blend; and then cooling and granulating the obtained blend.

**[0010]** Alternatively, the new polyolefin alloy can be produced by blending the components (A) and (B) and optionally utilized component (E); melting the blend; blending the components (C) and (D) into the melt, preferably with kneading of the blend; and then cooling and granulating the obtained blend.

**[0011]** The production of the polyolefin alloy can be effected in a mixer of any suitable type, for instance a continuous or batchwise mixer, although it is preferred to use an extruder.

**[0012]** Particularly suitable polypropylene materials (A) for use in the new polyolefin alloy are copolymers of propylene and ethylene. A particularly suitable polypropylene material is a copolymer of propylene and ethylene having a content of 5 to 25% by weight of polymerized ethylene units.

**[0013]** Suitable functionalized polypropylene materials (B) for use in the new polyolefin alloy are polypropylene homopolymers and copolymers of propylene and ethylene and/or butadiene (B), grafted with a compound selected from maleic anhydride, acrylic acid, acrylates and methacrylates, vinyl silanes and other vinyl compounds. Particularly good results are obtained by grafting maleic anhydride on the polypropylene material. The functionalized polypropylene material can have a melt index MI in the range of 5 to 250 g/10 min at 230°C/2.16 kg, more preferably in the range of 10 to 150 g/10 min at 230°C/2.16 kg.

**[0014]** Suitable minerals (C) for use in the polyolefin alloy of the invention are finely divided minerals which have been silanized with one or more of the aminosilanes traditionally used for surface treatment of talc. Particularly suitable minerals for use in the alloy after such silanizing treatment are wollastonite, kaolin, mica, calcium carbonate and talc, particularly talc. Preferably, the treated mineral has a mean particle size  $D_{50}$  in the range of 0.5 to 10  $\mu\text{m}$ , more preferably 1-6  $\mu\text{m}$ .

**[0015]** The silica gel material (D) which is used in the polyolefin alloy of the invention is preferably a fatty amide-treated, amorphous, synthetic silica gel containing 40 to 65% by weight of silica and 60 to 35% by weight of fatty acid amide.

**[0016]** Ethylene/propylene/polyene terpolymers (EPDM) that are particularly useful as an optional component in the polymer alloy of the invention are such terpolymers which have an ethylene content of 30 to 90% by weight and a flow, determined according to the Mooney method (ML 101°C), of 0 to 60, more preferably 0 to 50.

**[0017]** Although the invention is not meant to be limited by any particular theory regarding the mechanism behind the improved surface hardness and scratch resistance achieved with the new polyolefin alloy, chemical reaction seems to take place between the functionalized polypropylene material (B) and the surface-treated mineral (C), and between the functionalized polypropylene material (B) and the amorphous, fatty acid amide-treated silica gel (D).

**[0018]** The following examples illustrate the preparation of the new polyolefin alloys of the invention. The following properties of the prepared alloys were measured:

Modulus of elasticity: Measured at 23°C according to ISO 527 (MPa).

Notched Izod: Measured at -40°C according to ISO VSI 180/1A (kJ/m<sup>2</sup>).

Thermal shape stability (HDTA): Measured according to ISO 75 (°C).

Shrinkage: Calculated directly (in %) from measurements of length and width of a stamped square of a sheet of thickness 2 mm, moulded under given injection moulding conditions. The test sheets for each pair of Example illustrating the invention and Comparison Example were moulded under the same moulding conditions.

Scratch resistance: Measured with an Ericsson pen according to ISO 1518.

#### Example 1

**[0019]** An alloy on polypropylene basis was prepared from the following components:

A. A copolymer of propylene and ethylene containing 14% by weight of polymerized ethylene and having a melt

index MI of 8.0 g/10 min at 230°C/2.16 kg.

B. A polypropylene functionalized with maleic anhydride (MAH), containing 0.7% by weight of MAH and having a melt index MI of 200 g/10 min at 230°C/2.16 kg.

C. A talc the surface of which has been treated with 1.5 to 2.0% by weight of aminosilane, said talc having a density of 330 kg/m<sup>3</sup> and a particle size D<sub>50</sub> of 2 to 5 µm.

D. An amorphous, synthetic, fatty acid amide-treated silica gel, containing 40 to 50% by weight of fatty acid amide (essentially 13-docoseneamide), having a density of 300 kg/m<sup>3</sup> and a particle size D<sub>50</sub> of 2 to 4 µm.

E. A low crystallinity ethylene/propylene/polyene terpolymer (EPDM) containing 47% of polymerized ethylene and having a density of 870 kg/m<sup>3</sup> and melt index MI of 0.6 g/10 min at 230°C/2.16 kg.

**[0020]** The alloy was prepared in a "Werner & Pfleiderer" double screw extruder, type ZSK, having 57 mm co-rotating screws. Before and after the preparation, the hopper was flushed with nitrogen gas in order that the preparation should take place in an approximately inert atmosphere. The screw speed was 200 rpm and the rate of extrusion was 80 kg/h. All the raw material was introduced gravimetrically at feed point 1. The temperature profile of the extruder was maintained in the range of 210 to 230°C. The components added, the amounts thereof (in % by weight of the total blend) and the results are given in the table below. Fig. 1 shows the appearance of a test sample of the alloy after the scratch resistance having been measured with an Ericsson pen according to ISO 1518.

#### Example 2 (Comparison example)

**[0021]** The procedure of Example 1 was followed, with the exception that the fatty acid amide-treated silica gel (component D) was omitted. The added components, the amounts thereof (in % by weight of the total blend) and the results are given in the table below. Fig. 2 shows the appearance of a test sample of the alloy after the scratch resistance having been measured with an Ericsson pen according to ISO 1518.

#### Example 3

**[0022]** It was proceeded as in Example 1, with the exception that the amount of talc (component C) was increased from 10% by weight to 30% by weight. The added components, the amounts thereof (in % by weight of the total blend) and the results are given in the table below. Fig. 3 shows the appearance of a test sample of the alloy after the scratch resistance having been measured with an Ericsson pen according to ISO 1518.

#### Example 4 (Comparison example)

**[0023]** It was proceeded as in Example 2, with the exception that the amount of talc (component C) was increased from 10% by weight to 30% by weight. The added components, the amounts thereof (in % by weight of the total blend) and the results are given in the table below. Fig. 4 shows the appearance of a test sample of the alloy after the scratch resistance having been measured with an Ericsson pen according to ISO 1518.

Table

Preparation of alloys on polypropylene basis, having improved scratch resistance.

Ex.	PP <sup>1)</sup> (% wt)	PP-g- MAH <sub>2</sub> <sup>2)</sup> (% wt)	Talc <sup>3)</sup> (% wt)	Silica gel <sup>4)</sup> (% wt)	EPDM (% wt)	E-modu- lus (MPa)	Izod -40°C (J/m)	HDTA (°C)	Shrink- age (%)	Scratch resist. (7,5 N)
1	70	5	10	5	10	1450	60	52	1,3	3
2 (Comp.)	80	-	10	-	10	1600	50	54	1,3	0,5
3	50	5	30	5	10	2100	50	64	1,0	5
4 (Comp.)	60	-	30	-	10	2400	35	68	0,7	1

<sup>1)</sup> A copolymer of propylene and ethylene with 14% by weight of polymerized ethylene and a MI 8.0 g/10 min at 230°C/2.16 kg.

<sup>2)</sup> A polypropylene functionalized with MAH, having a MAH content of 0.7% by weight and a MI of 200 g/10 min at 230°C/2.16 kg.

<sup>3)</sup> A talc surface-treated with 1.5 - 2.0% by weight of aminosilane, having a density of 330 kg/m<sup>3</sup> and a particle size D<sub>50</sub> p<sub>a</sub> 2-5 μm.

<sup>4)</sup> An amorphous, synthetic, fatty acid amide-treated silica, containing 40-50% by weight of fatty acid amide, and having a density of 300 kg/m<sup>3</sup> and a particle size D<sub>50</sub> of 2-4 μm.

<sup>5)</sup> A low crystallinity ethylene/propylene/polyene terpolymer (EPI<sub>1</sub>M) containing 47% of polymerized ethylene, having a density of 870 kg/m<sup>3</sup> and a melt index MI of 0.6 g/10 min at 230°C/2.16 kg.

[0024] It can be seen from the results given in the above table, by comparing Example 1 illustrating the invention and Comparison Example 2 illustrating the prior art, that addition of 5% by weight of fatty acid amide-treated silica gel substantially improves the scratch resistance of the alloy, which increases from 0.5 to 3. This improvement is also clearly seen by comparing Fig. 1, which shows the surface of a test sample of the alloy of Example 1 after the scratch resistance having been measured, with Fig. 2, which is a similar picture of a test sample of the alloy of Example 2. The table further shows that the stiffness (E modulus) is somewhat reduced, whereas the notched bar impact (Izod) at -40°C and the thermal shape stability (HDTA) are improved with the new technology.

[0025] A similar comparison between the results obtained for the alloys of Example 3 and Example 4 (comparison example), in which examples 30% by weight of talc was used (vs. 10% by weight in Examples 1 and 2), shows that a substantial increase in the scratch resistance is achieved by adding 5% by weight of fatty acid amide-treated silica gel, said scratch resistance increasing from 1 to 5. The improvement is also clearly seen by comparing Fig. 3, which shows the surface of the new alloy of Example 3 after the scratch resistance having been measured, with Fig. 4, which is a similar picture of the alloy of Example 4. It also appears from the table that the E modulus and shrinkage values are somewhat reduced for the alloy of Example 3, whereas the notched bar impact (Izod) at -40°C and the thermal shape stability (HDTA) are improved with the new technology.

### Claims

1. A polyolefin alloy having improved surface hardness and scratch resistance, and having a melt index MI in the range of 0.1 to 50 g/10 min at 230°C/2.16 kg, particularly in the range of 3 to 40 g/10 min at 230°C/2.16 kg, **characterized** in that it is constituted by a blend of:

(A) 40 to 80% by weight of a polypropylene material consisting of a polypropylene homopolymer or a copolymer of propylene with ethylene and/or butadiene, which polypropylene material may have a content of polymerized ethylene and/or butadiene units of 5 to 35 mole% and has a molecular weight Mw of 100,000 to 300,000 and a melt index MI of 0.1 to 20 g/10 min at 230°C/2.16 kg,

(B) 1 to 10% by weight of a functionalized polypropylene material consisting of a grafted polypropylene homopolymer or copolymer of propylene with ethylene and/or butadiene, having a degree of grafting of 0.2 to 10% by weight,

(C) 1 to 50% by weight of a mineral, having a mean particle size of about 2.5 µm and a maximum particle size of 20 µm, and being surface-treated with 0.2 to 5% by weight of aminosilane,

(D) 1 to 15% by weight of amorphous fatty acid-treated silica gel, comprising 25 to 75% by weight of silica and 75 to 25% by weight of fatty acid amide,

(E) 0 to 40% by weight of an ethylene/propylene/-polyene terpolymer (EPDM) having a melt index MI in the range of 1 to 10 g/10 min at 230°C/2.16 kg and a Shore D hardness of 30 to 70.

2. A polyolefin alloy according to claim 1, **characterized** in that the functionalized polypropylene homopolymer or copolymer of propylene with ethylene and/or butadiene (B) is grafted with a compound selected from maleic anhydride, acrylic acid, acrylates and methacrylates, vinyl silanes and other vinyl compounds, preferably maleic anhydride.

3. A polyolefin alloy according to claim 1 or 2, **characterized** in that the polypropylene material (A) is a copolymer of propylene and ethylene and has a content of 5 to 25% by weight of polymerized ethylene units.

4. A polyolefin alloy according to any of claims 1 to 3, **characterized** in that it is constituted by a blend of:

60 to 80 % by weight of (A);

2,5 to 7,5 % by weight of (B);

7,5 to 35 % by weight of (C);

2,5 to 7,5 % by weight of (D);

0 to 25 % by weight of (E).

5. A polyolefin alloy according to any of claims 1 to 4, **characterized** in that the functionalized polypropylene material (B) has a degree of grafting of 0.5 to 2% by weight.

6. A polyolefin alloy according to any of claims 1 to 5, **characterized** in that the surface-treated mineral (C) has been surface-treated with about 1% by weight of amino silane.

7. A polyolefin alloy according to any of claims 1 to 6, **characterized** in that the mineral (C) is selected from wollastonite, kaolin, mica, calcium carbonate and talc.
8. A polyolefin alloy according to claim 7, **characterized** in that the mineral (C) is talc.
9. A process for producing a polyolefin alloy according to any of claims 1 to 8, **characterized** by the steps of blending the components (A), (B), (C) and (D) and optionally utilized component (E); melting and preferably kneading the blend; and then cooling and granulating the obtained blend.
10. A process for producing a polyolefin alloy according to any of claims 1 to 8, **characterized** by the steps of blending the components (A) and (B) and optionally utilized component (E); melting the blend; blending the components (C) and (D) into the melt, preferably with kneading of the blend; and then cooling and granulating the obtained blend.

## Patentansprüche

1. Polyolefinlegierung mit verbesserter Oberflächenhärte und Kratzfestigkeit und mit einem Schmelzindex MI im Bereich von 0,1 bis 50 g/10 min bei 230°C/2,16 kg, insbesondere im Bereich von 3 bis 40 g/10 min bei 230°C/2,16 kg, dadurch gekennzeichnet, daß sie sich zusammensetzt aus einer Mischung aus:

(A) 40 bis 80 Gew. % eines Polypropylen-Materials, bestehend aus einem Polypropylen-Homopolymer oder einem Copolymer aus Propylen mit Ethylen und/oder Butadien, wobei das Polypropylen-Material einen Gehalt an polymerisierten Ethylen- und/oder Butadien-Einheiten von 5 bis 35 Mol% aufweisen kann und ein Molekulargewicht Mw von 100.000 bis 300.000 sowie einen Schmelzindex MI von 0,1 bis 20 g/10 min bei 230°C/2,16 kg aufweist,

(B) 1 bis 10 Gew.% eines funktionalisierten Polypropylen-Materials, das aus einem gepfropften Polypropylen-Homopolymer oder Copolymer aus Propylen mit Ethylen und/oder Butadien besteht und einen Pfropfungsgrad von 0,2 bis 10 Gew. % aufweist,

(C) 1 bis 50 Gew. % eines Minerals, das eine mittlere Teilchengröße von ungefähr 2,5 µm und eine maximale Teilchengröße von 20 µm aufweist und mit 0,2 bis 5 Gew. % Aminosilan oberflächenbehandelt wird,

(D) 1 bis 15 Gew. % amorphen fettsäurebehandelten Silicagels, welches 25 bis 75 Gew. % Silicamasse und 75 bis 25 Gew. % Fettsäureamid aufweist,

(E) 0 bis 40 Gew. % eines Ethylen/Propylen/Polyen-Terpolymers (EPDM) mit einem Schmelzindex MI im Bereich von 1 bis 10 g/10 min bei 230°C/2,16 kg und einer Shore-D-Härte von 30 bis 70.

2. Polyolefinlegierung nach Anspruch 1, dadurch gekennzeichnet, daß das funktionalisierte Polypropylenhomopolymer oder Copolymer aus Propylen mit Ethylen und/oder Butadien (B) mit einer Verbindung aus der Gruppe umfassend Maleinsäureanhydrid, Acrylsäure, Acrylate und Methacrylate, Vinylsilane und anderen Vinylverbindungen, vorzugsweise mit Maleinsäureanhydrid, gepfropft wird.

3. Polyolefinlegierung nach Anspruch 1 oder 2, dadurch gekennzeichnet, daß das Polypropylen-Material (A) ein Copolymer aus Propylen und Ethylen ist und einen Gehalt von 5 bis 25 Gew. % polymerisierte Ethyleneinheiten aufweist.

4. Polyolefinlegierung nach irgend einem der Ansprüche 1 bis 3, dadurch gekennzeichnet, daß sie sich zusammensetzt aus einer Mischung aus:

60 bis 80 Gew.% von (A);  
2,5 bis 7,5 Gew. % von (B);  
7,5 bis 35 Gew.% von (C);  
2,5 bis 7,5 Gew.% von (D);  
0 bis 25 Gew.% von (E).

5. Polyolefinlegierung nach irgend einem der Ansprüche 1 bis 4, dadurch gekennzeichnet, daß das funktionalisierte Polypropylen-Material (B) einen Pfropfungsgrad von 0,5 bis 2 Gew. % aufweist.

6. Polyolefinlegierung nach irgend einem der Ansprüche 1 bis 5, dadurch gekennzeichnet, daß das oberflächenbehandelte Mineral (C) mit ungefähr 1 Gew.% Aminosilan oberflächenbehandelt wurde.

7. Polyolefinlegierung nach irgend einem der Ansprüche 1 bis 6, dadurch gekennzeichnet, daß das Mineral (C) aus der Gruppe umfassend Wollastonit, Kaolin, Glimmer, Calciumcarbonat und Talk ausgewählt wird.
8. Polyolefinlegierung nach Anspruch 7, dadurch gekennzeichnet, daß das Mineral (C) Talk ist.
9. Verfahren zur Herstellung einer Polyolefinlegierung nach irgend einem der Ansprüche 1 bis 8, gekennzeichnet durch die Schritte des Mischens der Komponenten (A), (B), (C) und (D) und der wahlweise verwendeten Komponente (E); des Schmelzens und vorzugsweise des Knetens der Mischung; und daraufhin des Kühlens und Granulierens der gewonnenen Mischung.
10. Verfahren zur Herstellung einer Polyolefinlegierung nach einem beliebigen der Ansprüche 1 bis 8, gekennzeichnet durch die Schritte des Mischens der Komponenten (A) und (B) und der wahlweise verwendeten Komponente (E); des Schmelzens der Mischung; des Einmischens der Komponenten (C) und (D) in die Schmelze, vorzugsweise mit Kneten der Mischung; und daraufhin des Kühlens und Granulierens der gewonnenen Mischung.

## Revendications

1. Alliage polyoléfinique doté d'une dureté superficielle et d'une résistance à la rayure améliorées, et présentant un indice de fusion MI dans l'intervalle de 0,1 à 50 g/10 min à 230°C/2,16 kg, en particulier dans l'intervalle de 3 à 40 g/10 min à 230°C/2,16kg, caractérisé en ce qu'il est constitué d'un mélange de :

(A) 40 à 80% en poids d'un matériau de polypropylène composé d'un homopolymère de polypropylène ou d'un copolymère de propylène et d'éthylène et/ou de butadiène, lequel matériau de polypropylène peut avoir une teneur en unités polymérisés d'éthylène et/ou de butadiène de 5 à 35% en mole et a un poids moléculaire Mw de 100 000 à 300 000 et un indice de fusion MI de 0,1 à 20 g/10 min à 230°C/2,16 kg;

(B) 1 à 10% en poids d'un matériau de polypropylène fonctionnalisé composé d'un homopolymère de polypropylène greffé ou d'un copolymère de propylène et d'éthylène et/ou de butadiène, présentant un degré de greffage de 0,2 à 10% en poids;

(C) 1 à 50% en poids d'un minéral, présentant une taille particulière moyenne d'environ 2,5 µm et une taille particulière maximale de 20 µm, et ayant subi un traitement de surface avec 0,2 à 5% en poids d'aminosilane;

(D) 1 à 15% en poids de gel de silice amorphe traité avec un acide gras, comprenant 25 à 75% en poids de silice et 75 à 25% en poids d'amide d'acide gras, et

(E) 0 à 40% en poids d'un terpolymère d'éthylène/propylène/polyène (EPDM) présentant un indice de fusion MI dans l'intervalle de 1 à 10 g/10 min à 230°C/2,16 kg et une dureté Shore D de 30 à 70.

2. Alliage polyoléfinique suivant la revendication 1, caractérisé en ce que l'homopolymère de polypropylène fonctionnalisé ou le copolymère de propylène et d'éthylène et/ou de butadiène (B) est greffé avec un composé sélectionné parmi l'anhydride maléique, l'acide acrylique, les acrylates et méthacrylates, les silanes de vinyle et d'autres composés vinyliques, de préférence l'anhydride maléique.

3. Alliage polyoléfinique suivant la revendication 1 ou 2, caractérisé en ce que le matériau de polypropylène (A) est un copolymère de propylène et d'éthylène et a une teneur de 5 à 25% en poids en unités d'éthylène polymérisé.

4. Alliage polyoléfinique suivant l'une quelconque des revendications 1 à 3, caractérisé en ce qu'il est composé d'un mélange de :

60 à 80% en poids de (A);

2,5 à 7,5% en poids de (B);

7,5 à 35% en poids de (C);

2,5 à 7,5% en poids de (D), et

0 à 25% en poids de (E).

5. Alliage polyoléfinique suivant l'une quelconque des revendications 1 à 4, caractérisé en ce que le matériau de polypropylène fonctionnalisé (B) présente un degré de greffage de 0,5 à 2% en poids.

6. Alliage polyoléfinique suivant l'une quelconque des revendications 1 à 5, caractérisé en ce que le minéral ayant subi un traitement de surface (C) a subi un traitement de surface avec environ 1% en poids d'aminosilane.



7. Alliage polyoléfinique suivant l'une quelconque des revendications 1 à 6, caractérisé en ce que le minéral (C) est sélectionné parmi la wollastonite, le kaolin, le mica, le carbonate de calcium et le talc.
8. Alliage polyoléfinique suivant la revendication 7, caractérisé en ce que le minéral (C) est du talc.
9. Procédé de production d'un alliage polyoléfinique suivant l'une quelconque des revendications 1 à 8, caractérisé par les étapes de mélange des composants (A), (B), (C) et (D) et le composant utilisé facultativement (E); de fusion et de préférence de malaxage du mélange, et ensuite de refroidissement et de granulation du mélange obtenu.
10. Procédé de production d'un alliage polyoléfinique suivant l'une quelconque des revendications 1 à 8, caractérisé par les étapes de mélange des composants (A) et (B) et du composant utilisé facultativement (E); de fusion; de mélange des composants (C) et (D) à la matière fondue, et de préférence avec le malaxage du mélange, et ensuite le refroidissement et la granulation du mélange obtenu.

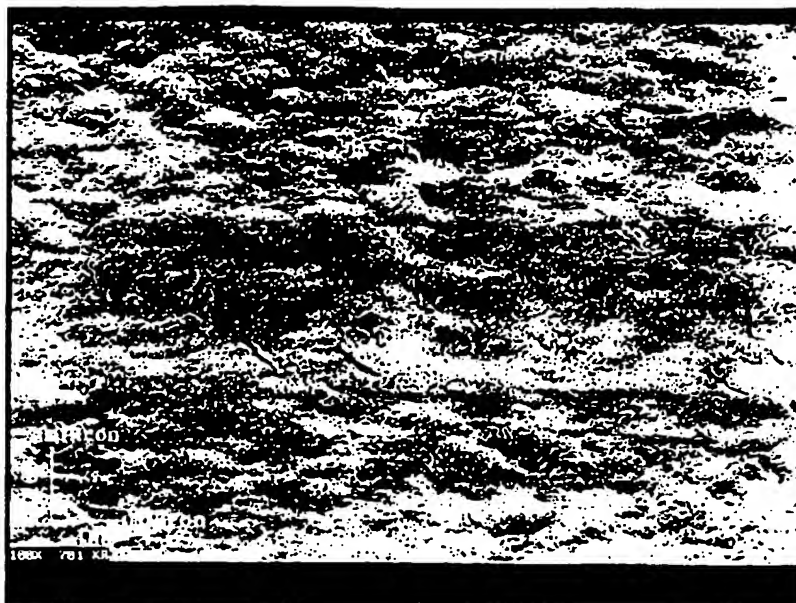


FIG. 1

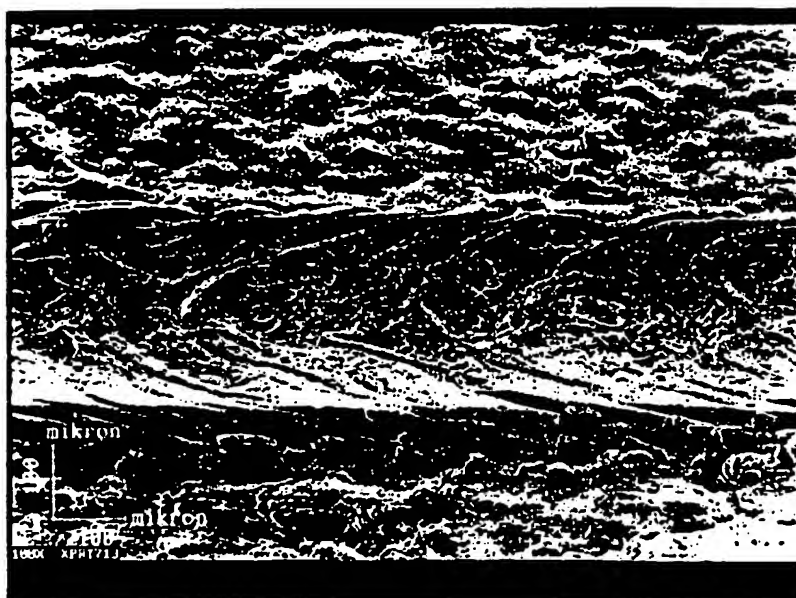


FIG. 2

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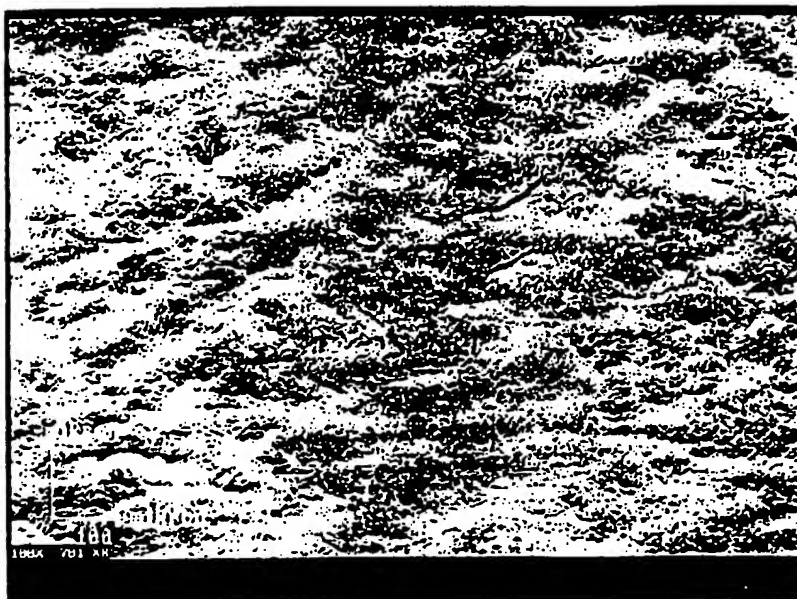


FIG. 3

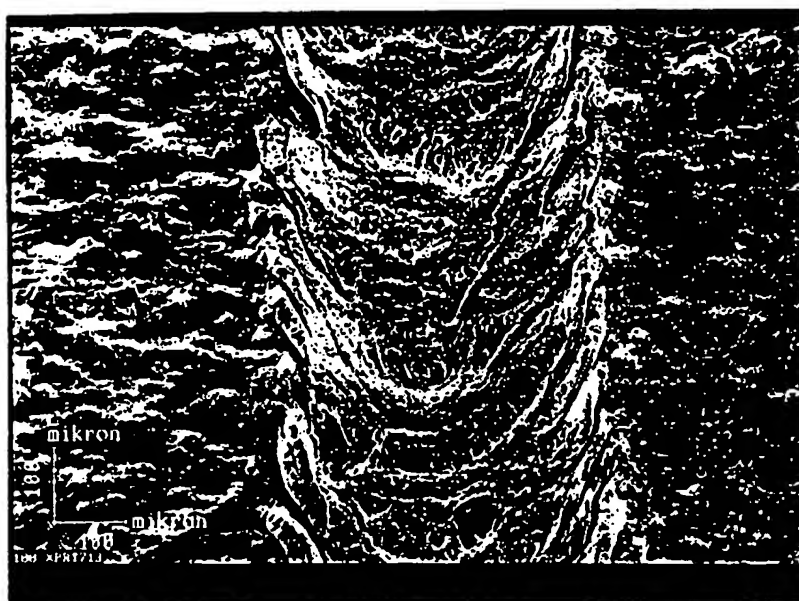


FIG. 4

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